

Problem 2D.2

Drainage of liquids⁹ (see Fig. 2D.2). How much liquid clings to the inside surface of a large vessel when it is drained? As shown in the figure there is a thin film of liquid left behind on the wall as the liquid level in the vessel falls. The local film thickness is a function of both z (the distance down from the initial liquid level) and t (the elapsed time).

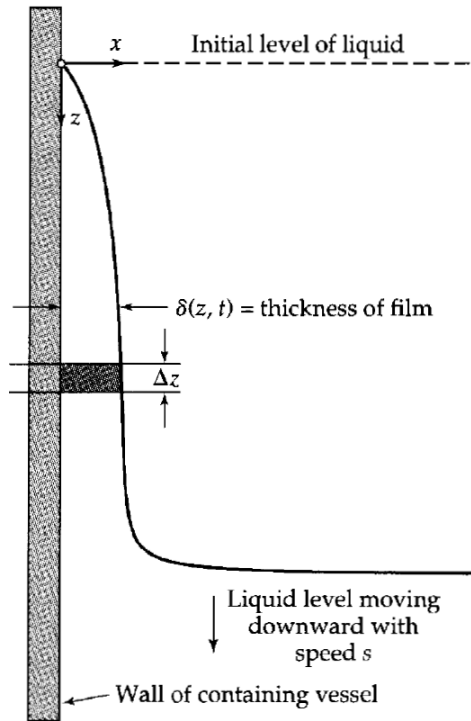


Fig. 2D.2 Clinging of a viscous fluid to wall of vessel during draining.

- (a) Make an unsteady-state mass balance on a portion of the film between z and $z + \Delta z$ to get

$$\frac{\partial}{\partial z} \langle v_z \rangle \delta = -\frac{\partial \delta}{\partial t} \quad (2D.2-1)$$

- (b) Use Eq. 2.2-18 and a quasi-steady-assumption to obtain the following first-order partial differential equation for $\delta(z, t)$:

$$\frac{\partial \delta}{\partial t} + \frac{\rho g}{\mu} \delta^2 \frac{\partial \delta}{\partial z} = 0 \quad (2D.2-2)$$

- (c) Solve this equation to get

$$\delta(z, t) = \sqrt{\frac{\mu}{\rho g} \frac{z}{t}} \quad (2D.2-3)$$

What restrictions have to be placed on this result?

Solution

⁹J. J. van Rossum, *Appl. Sci. Research*, **47**, 121-144 (1958); see also V. G. Levich, *Physicochemical Hydrodynamics*, Prentice-Hall, Englewood Cliffs, N.J. (1962), Chapter 12.

Part (a)

The law of conservation of mass states that matter is neither created nor destroyed. The same amount of fluid that enters a shell per unit time must leave at that same rate; otherwise, fluid will build up or accumulate within the shell. The mathematical expression for this idea, a mass balance, is as follows.

$$\text{rate of mass in} - \text{rate of mass out} = \text{rate of mass accumulation}$$

Because of viscosity, the fluid in this problem doesn't flow freely. Some of it gets stuck to the

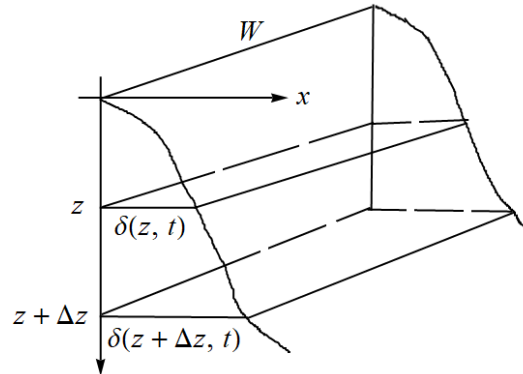


Figure 1: This is the shell over which the mass balance is made for liquid draining.

wall, so the rate of accumulation is not zero. Mass flows in at z and out at $z + \Delta z$, so with the shell in Figure 1 the mass balance becomes

$$\left. \frac{dm}{dt} \right|_z - \left. \frac{dm}{dt} \right|_{z+\Delta z} = \left. \frac{dm}{dt} \right|_{\text{shell}}.$$

Mass is density times volume.

$$\left. \frac{d(\rho V)}{dt} \right|_z - \left. \frac{d(\rho V)}{dt} \right|_{z+\Delta z} = \left. \frac{d(\rho V)}{dt} \right|_{\text{shell}}$$

As the density is assumed to be constant, it can be pulled out of each derivative and cancelled.

$$\left. \frac{dV}{dt} \right|_z - \left. \frac{dV}{dt} \right|_{z+\Delta z} = \left. \frac{dV}{dt} \right|_{\text{shell}}$$

For the left-hand side, the volumetric flow rate is the average velocity times the cross-sectional area that the fluid flows through.

$$\langle v \rangle|_z [A] - \langle v \rangle|_{z+\Delta z} [A] = \left. \frac{dV}{dt} \right|_{\text{shell}}$$

The cross-sectional areas at z and $z + \Delta z$ are $W\delta(z, t)$ and $W\delta(z + \Delta z, t)$, respectively.

$$\langle v \rangle|_z [W\delta(z, t)] - \langle v \rangle|_{z+\Delta z} [W\delta(z + \Delta z, t)] = \left. \frac{dV}{dt} \right|_{\text{shell}}$$

Factor $-W$ from the left side.

$$-W[\langle v \rangle|_{z+\Delta z} \delta(z + \Delta z, t) - \langle v \rangle|_z \delta(z, t)] = \left. \frac{dV}{dt} \right|_{\text{shell}}$$

For the right-hand side, an expression for the volume of the shell from z to $z + \Delta z$ can be obtained by integrating the cross-sectional area over that interval.

$$V|_{\text{shell}} = \int_z^{z+\Delta z} A(s) ds$$

We get

$$-W[\langle v \rangle|_{z+\Delta z} \delta(z + \Delta z, t) - \langle v \rangle|_z \delta(z, t)] = \frac{d}{dt} \int_z^{z+\Delta z} [W\delta(s, t)] ds.$$

Now take the limit as $\Delta z \rightarrow 0$. It is assumed that δ is continuous and differentiable.

$$\lim_{\Delta z \rightarrow 0} -W[\langle v \rangle|_{z+\Delta z} \delta(z + \Delta z, t) - \langle v \rangle|_z \delta(z, t)] = \lim_{\Delta z \rightarrow 0} \frac{d}{dt} \int_z^{z+\Delta z} [W\delta(s, t)] ds$$

Bring the limit inside the derivative.

$$-W \lim_{\Delta z \rightarrow 0} [\langle v \rangle|_{z+\Delta z} \delta(z + \Delta z, t) - \langle v \rangle|_z \delta(z, t)] = \frac{d}{dt} \lim_{\Delta z \rightarrow 0} \int_z^{z+\Delta z} [W\delta(s, t)] ds$$

The interval of integration becomes so small that the integrand is essentially constant and can be pulled in front of the integral.

$$-W \lim_{\Delta z \rightarrow 0} [\langle v \rangle|_{z+\Delta z} \delta(z + \Delta z, t) - \langle v \rangle|_z \delta(z, t)] = \frac{d}{dt} \lim_{\Delta z \rightarrow 0} [W\delta(z, t)] \int_z^{z+\Delta z} ds$$

Evaluate the integral.

$$-W \lim_{\Delta z \rightarrow 0} [\langle v \rangle|_{z+\Delta z} \delta(z + \Delta z, t) - \langle v \rangle|_z \delta(z, t)] = \frac{d}{dt} \lim_{\Delta z \rightarrow 0} [W\delta(z, t)] \Delta z$$

W and Δz are constants with respect to time.

$$-W \lim_{\Delta z \rightarrow 0} [\langle v \rangle|_{z+\Delta z} \delta(z + \Delta z, t) - \langle v \rangle|_z \delta(z, t)] = W \frac{\partial \delta}{\partial t} \left(\lim_{\Delta z \rightarrow 0} \Delta z \right)$$

Divide both sides by $W\Delta z$.

$$-\lim_{\Delta z \rightarrow 0} \frac{\langle v \rangle|_{z+\Delta z} \delta(z + \Delta z, t) - \langle v \rangle|_z \delta(z, t)}{\Delta z} = \frac{\partial \delta}{\partial t}$$

The limit on the left is how the first derivative of $\langle v \rangle \delta$ with respect to z is defined.

$$-\frac{\partial}{\partial z} \langle v \rangle \delta = \frac{\partial \delta}{\partial t}$$

Therefore,

$$\frac{\partial}{\partial z} \langle v \rangle \delta = -\frac{\partial \delta}{\partial t}.$$

Part (b)

Eq. 2.2-18 gives the velocity distribution for a fluid flowing down an inclined plane.

$$\begin{aligned} v_z &= \frac{\rho g \delta^2 \cos \beta}{2\mu} \left[1 - \left(\frac{x}{\delta} \right)^2 \right] \\ &= \frac{\rho g \cos \beta}{2\mu} (\delta^2 - x^2) \end{aligned} \quad (2.2-18)$$

To adapt the formula to this problem, set $\beta = 0$ because the wall is vertical. To obtain the average velocity $\langle v \rangle$, integrate this velocity over the cross-sectional area that the fluid flows through and then divide by that area.

$$\begin{aligned} \langle v \rangle &= \frac{1}{A} \int v_z dA \\ &= \frac{1}{W\delta(z,t)} \int_0^{\delta(z,t)} v_z(W dx) \\ &= \frac{1}{\delta(z,t)} \int_0^{\delta(z,t)} v_z dx \\ &= \frac{1}{\delta} \int_0^{\delta} \frac{\rho g}{2\mu} (\delta^2 - x^2) dx \\ &= \frac{\rho g}{2\mu\delta} \left(\delta^2 x - \frac{x^3}{3} \right) \Big|_0^{\delta} \\ &= \frac{\rho g}{2\mu\delta} \left(\frac{2\delta^3}{3} \right) \\ &= \frac{\rho g \delta^2}{3\mu} \end{aligned}$$

Substitute this formula for $\langle v \rangle$ into the mass balance.

$$\begin{aligned} \frac{\partial}{\partial z} \left(\frac{\rho g \delta^2}{3\mu} \right) \delta &= -\frac{\partial \delta}{\partial t} \\ \frac{\partial}{\partial z} \left(\frac{\rho g \delta^3}{3\mu} \right) &= -\frac{\partial \delta}{\partial t} \\ \frac{\rho g \delta^2}{\mu} \frac{\partial \delta}{\partial z} &= -\frac{\partial \delta}{\partial t} \end{aligned}$$

Therefore, we obtain a nonlinear first-order partial differential equation (PDE) for the film thickness.

$$\frac{\partial \delta}{\partial t} + \frac{\rho g}{\mu} \delta^2 \frac{\partial \delta}{\partial z} = 0$$

Part (c)

For a function of two variables $\delta = \delta(z, t)$, its differential is defined as

$$d\delta = \frac{\partial\delta}{\partial z} dz + \frac{\partial\delta}{\partial t} dt.$$

Divide both sides by dt .

$$\frac{d\delta}{dt} = \frac{\partial\delta}{\partial z} \frac{dz}{dt} + \frac{\partial\delta}{\partial t}$$

This equation is marvelous because it tells us the relationship between an ordinary derivative and the partial derivatives of a function. Comparing the PDE we have with this equation, we see that along the curves in the tz -plane (known as characteristics) defined by

$$\frac{dz}{dt} = \frac{\rho g}{\mu} \delta^2, \quad (1)$$

the PDE simplifies to an ordinary differential equation (ODE),

$$\frac{d\delta}{dt} = 0. \quad (2)$$

Integrate both sides of equation (2) with respect to t to solve for δ .

$$\delta = f(\xi),$$

where f is an arbitrary function and ξ is a coordinate along the characteristics. ξ can be written in terms of z and t by solving equation (1). Equation (2) tells us that δ is a constant with respect to time along the characteristics, so equation (1) can be solved by integrating both sides with respect to t .

$$z = \frac{\rho g}{\mu} \delta^2 t + \xi$$

Solve for ξ .

$$\xi = z - \frac{\rho g}{\mu} \delta^2 t$$

Thus, the general solution for δ is

$$\delta(z, t) = f\left(z - \frac{\rho g}{\mu} \delta^2 t\right),$$

though this is of little interest to us. Since the origin of the coordinate system is chosen so that the film thickness starts to develop at $z = 0$, the solution on the $\xi = 0$ characteristic is the one we care about.

$$0 = z - \frac{\rho g}{\mu} \delta^2 t$$

Therefore,

$$\delta(z, t) = \sqrt{\frac{\mu z}{\rho g t}}.$$

The solution only applies above the liquid level: $z > 0$, $t > 0$, and $z < st$. This can be written compactly as $0 < z < st$.

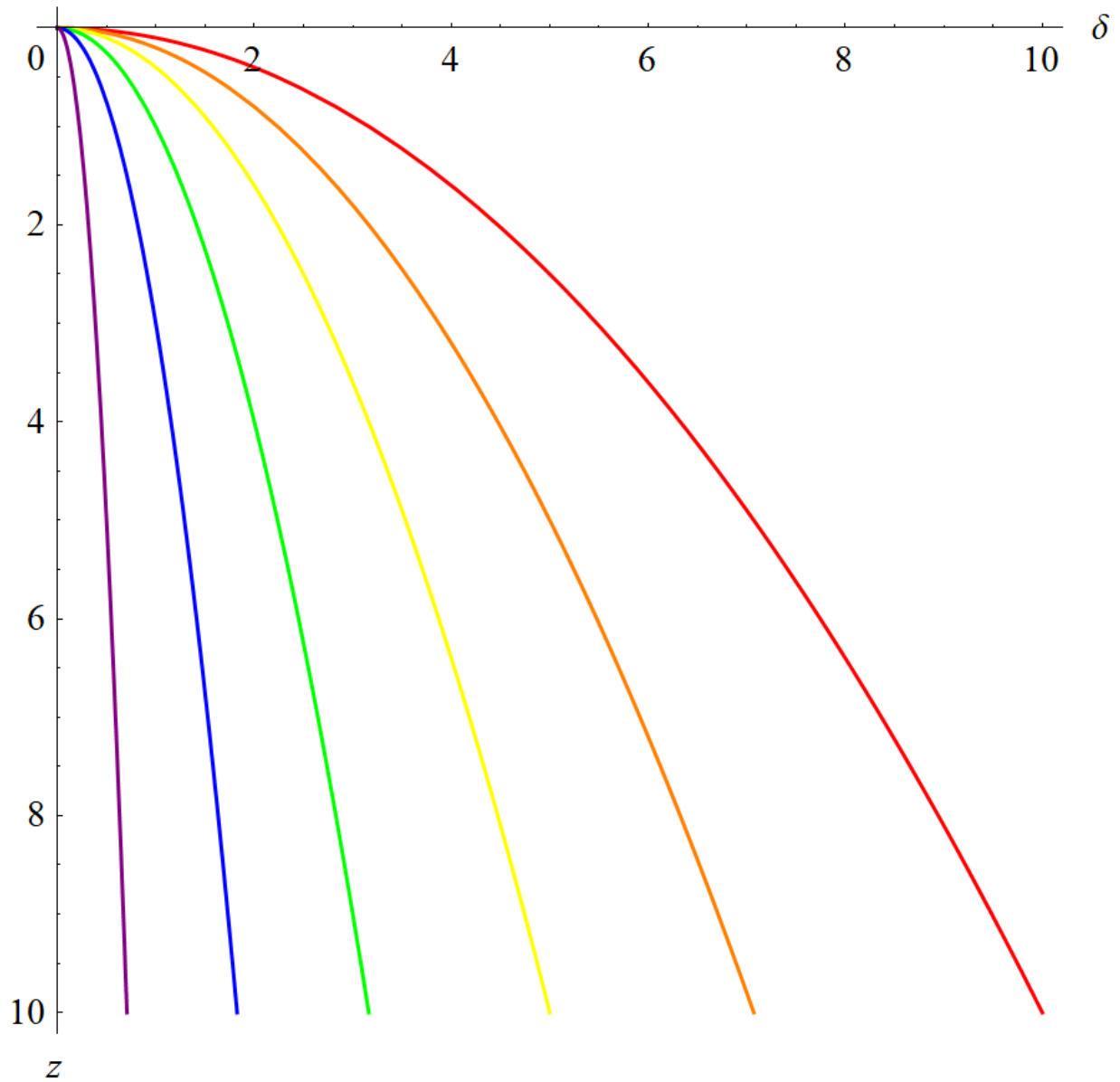


Figure 2: This is a plot of the film thickness δ vs. z at various times with $\mu/\rho g$ set equal to 1. The curves in red, orange, yellow, green, blue, and purple correspond to t equal to 0.1, 0.2, 0.4, 1, 3, and 20, respectively.